

# ECO-Design and Topology optimization

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October 21, 2024



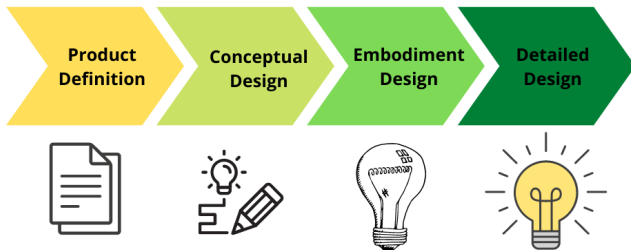
# Objectives

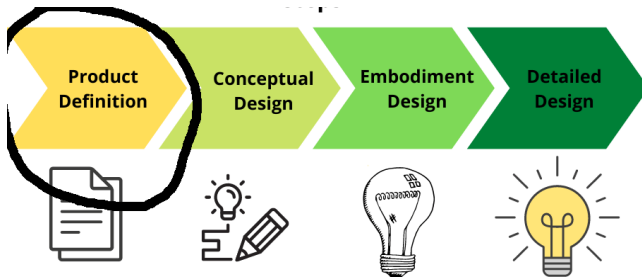
## Objectives

- To introduce the Conceptual Design Tools;
- Chose a simple but representative case study;
- Show the software usage for calculation of multi material truss structures mechanical eco-design parameter.
- Truss Topology Optimization or Gradient base Design of Steel-Timber Structures for Environmental Objectives;
- Project definitions.

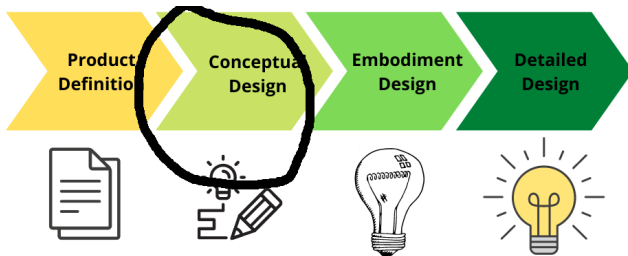
What is the conceptual mechanical/Structural Design?

A product design process is the sequence of steps an engineer employs to formulate, design, and manufacture a product or structure.



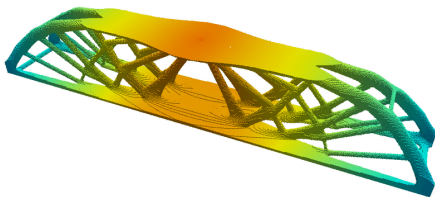
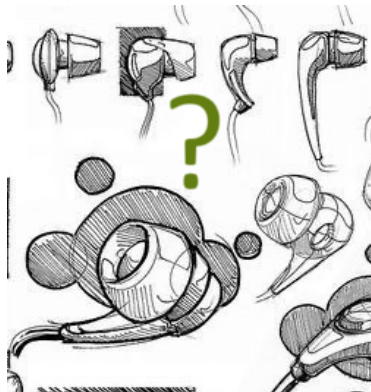


- A written request with a problem statement - Clients, Marketing ...;
- All Product requirements must be clarify in detail;
- It ensures that the engineers and designers understand the requirement of the product;

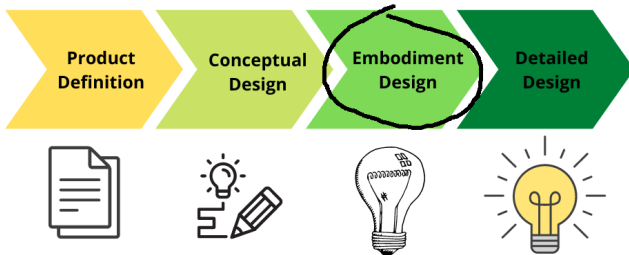


- Clarify the problem;
- Search externally;
- Search internally;
- Explore systematically;
- Reflection and choosing the concept;

In this case, some non intuitive solutions or innovative concepts may not be found. Topology Optimization is an option to find non intuitive solutions.



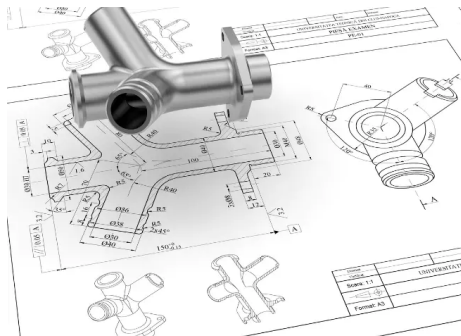
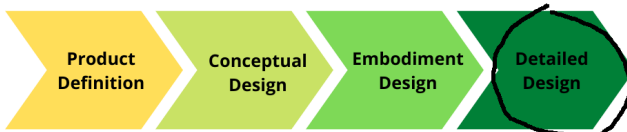




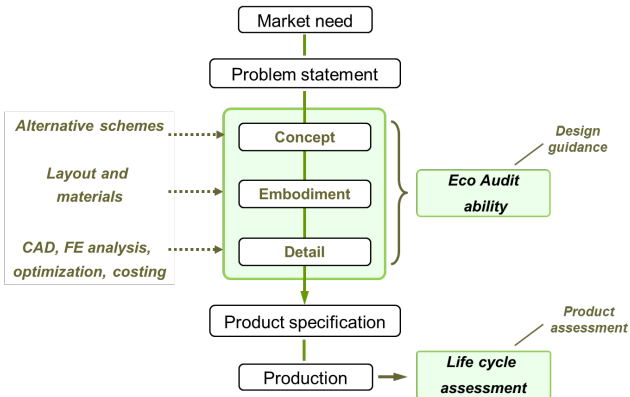
- Product architecture;
- Design configuration (Topology Optimization);



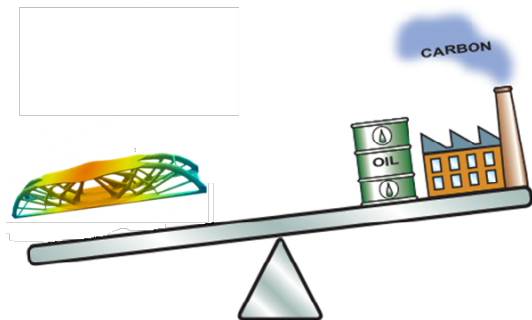
- Parametric design



The ECO-Design requirements can be considered in the phase of Conceptual - Embodiment - Detailed Design.



The goal is coupled the topological optimization and/or numerical simulation techniques with ECO-Design requirements in the Conceptual Design phase.



Chosen ECO-design indicator  $>$   $CO_2$  carbon footprint

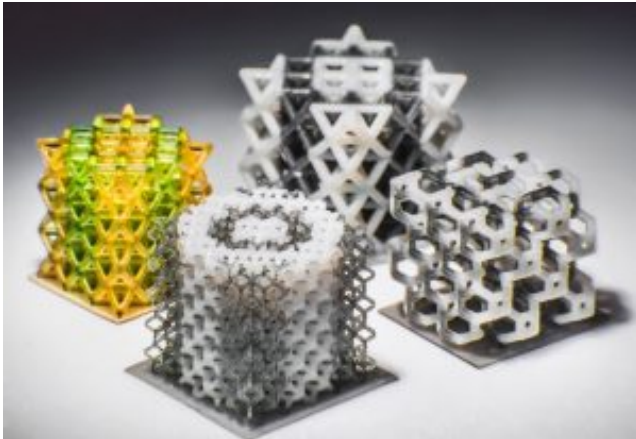
Problems Definitions > Simple but representative structure

To introduce this method, we consider the case of multi-material structures, for example a Truss build with steel mixed with parts processed using wood, as shown in figures



Figure: Metal Timber Structures

# Metamaterials Design - Multi-material micro-lattice polymeric structures fabricated using 3D printing



## The chosen problems: Timber-Steel Truss

Properties taken for timber and steel in the current work and the ratio of each property taken as steel/timber (e.g.  $E_{steel}/E_{timber}$ ).

Property		Steel	Timber	Property ratio
$E$	(GPa)	200	11	18.2
$\sigma_y$	(MPa)	$\pm 345$	$-8.6/ + 6.6$	40.1/52.3
$\rho$	( $\text{kg}/\text{m}^3$ )	7870	570	13.8
$ECC$	( $\text{kg}_{\text{CO}_2\text{e}}/\text{kg}_{\text{material}}$ )	1.45	0.42	3.5

Truss Topology Optimization of Steel-Timber Structures for Embodied Carbon Objectives. Ho Yin Ernest Ching Master of Science - MIT 2020



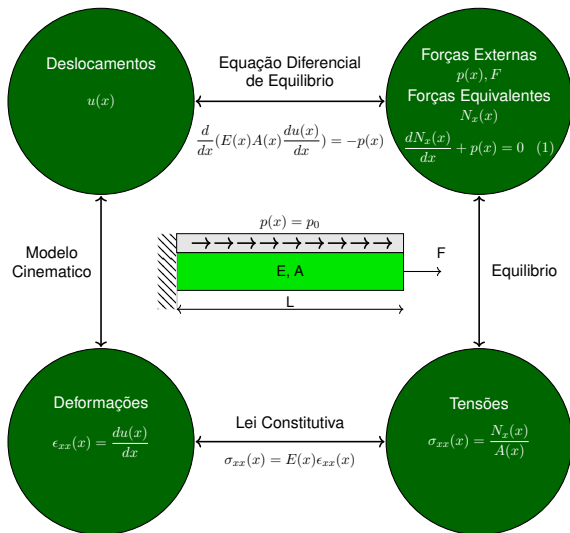
## Truss modeling and solution using finite element method

Formulation of static equilibrium equation of 2D truss using the finite element method. The state variables for each element can be calculate: volume, displacements, forces, stress.

The principal steps that will be remember are:

- Equilibrium equation;
- Discretization and approximation of the solution using Finite Element Method;
- Assemblage of the global system and Local to global transformation.
- Solve the discrete equilibrium equation to find nodal displacements.
- Post processing to evaluate the stresses, forces, weights,  $CO_2$  embodied, etc

# Equilibrium Differential equation for bar problems



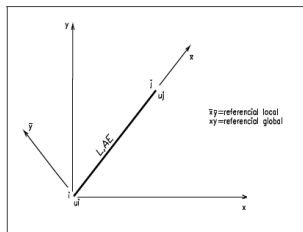
## Summary - bar problem

Find  $u(x)$  such that:

$$\left\{ \begin{array}{ll} EA \frac{d^2 u(x)}{dx^2} + p(x) = 0 & \text{in } \Omega \\ \text{sujeito a:} & \\ u = \bar{u} & \text{in } \Gamma_1 \\ \frac{\partial u}{\partial x} = \frac{\bar{F}}{EA} & \text{in } \Gamma_2 \end{array} \right.$$

## Finite Element Discretization - 2D Truss problem

The local and global coordinate system are  $(\bar{x}, \bar{y})$  and  $(x, y)$ .



The displacement vector  $u$  is:

$$u = \{ u_1, v_1, u_2, v_2 \}$$

Using  $\cos\theta = \lambda$  e  $\sin\theta = \mu$ , the elemental bar matrix can be written as:

$$[K] = \frac{AE}{L} \begin{bmatrix} \lambda^2 & & & \text{Sim.} \\ \lambda\mu & \mu^2 & & \\ -\lambda^2 & -\lambda\mu & \lambda^2 & \\ -\lambda\mu & -\mu^2 & \lambda\mu & \mu^2 \end{bmatrix} \quad (1)$$

and the force vector for one element:

$$F = \{ F_{ix}, F_{iy}, F_{jx}, F_{jy} \}$$

with all forces in the global  $(x, y)$  .

After Assemblage procedure, we can find the stiffness matrix and load vector for truss as shown bellow:

$$[Kg]\{ug\} = \{Fg\} \quad (2)$$

Show the software usage for calculation of multi material truss structures mechanical eco-design parameter.

**Tutorial Presentation**

## Matlab script

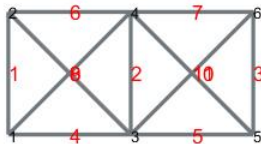
Implementation and testes of a simple truss using a Matlab script. Code Directory» ECO-TOP-2.m

The matlab implementation can be divided in the following tasks:

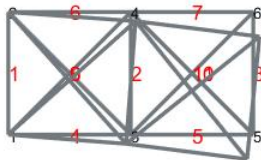
- Data base: node coordinates, elemental incidences, geometric and material properties
- Boundary conditions and load cases.
- Elemental properties: stiffness matrices and load vectors.
- Assemblage, boundary conditions ans solve.
- Post processing.

One script has been developed, to simulated the static equilibrium conditions, considering a cantilever boundary conditions, as represented in Figure (2). Two mesh generators have been developed. The first one for a X reinforced truss and, the second mesh generator all bar are connected with all nodes.

**Finite Element Mesh**



**Finite Element Mesh & Max. Displacement [m] = 0.00039142**





## Multi material Truss - Mechanical and Ecological variables

Implementation of a typical truss 2D case, and evaluate local/global indicator:

strain energies/compliance,

Embodied carbon Coefficients of the structure and

stress for each bars.

Compare the results of a steel truss with a timber/steel truss and timber trusses.

The second part of this implementation are related with the pos-processing of variables.

- $\mathbf{u}_g$  the nodal displacements;
- $\sigma_{xx}$  the elemental stress;
- $C = \mathbf{F}_g^T \mathbf{u}_g$  the structure Compliance ;
- $C_e = \mathbf{u}_e^T \mathbf{K}_e \mathbf{u}_e$  the elemental compliance;
- $\frac{dC}{dA_e}$  the sensitivity number;
- $W_e = \rho_e A_e L_e$  the elemental weight;
- $Wt = \sum W_e$  the weight of the structure;
- $ECC$  the material Embodied Carbon coefficient;
- $ECC_e = \rho_e A_e L_e ECC$  the elemental Embodied Carbon Coefficient.

In figure (3) we can observe one example with two materials and in figure (26) we can see the displacements and bar stress for a simple supported beam case.

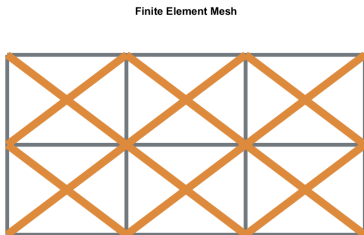
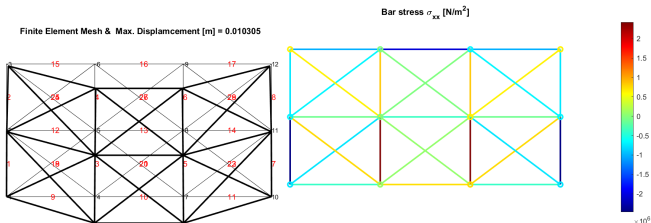


Figure: Steel(gray)/Timber(brown) truss



# Truss Topology Optimization or Gradient base Design of Steel-Timber Structures

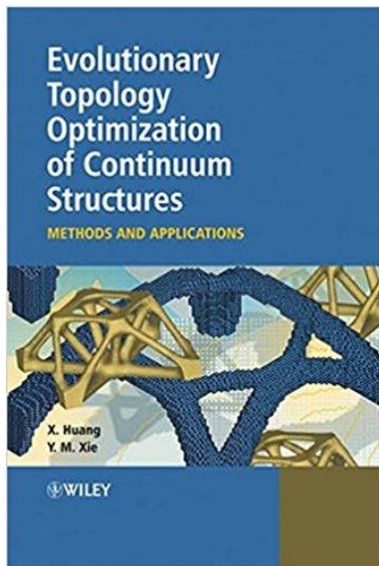
## Evolutionary Compliance Optimization: An heuristic Method

- We perform a single-material truss topology optimization for minimum compliance with weight and box constraints.
- The limits  $A_{min}$  and  $A_{max}$  cross section area variables are defined by the user.
- Formulation and sensitivity analysis, algorithm, implementation and tests are performed.

## BESO heuristic Method - characteristics

- Method was inspired in the nature evolution: Bones, plants, etc
- It can be applied for different Criteria: Stress, Compliance, Natural frequencies, Eco-design functions, etc
- This version of the Evolutionary method have been proposed by Xie, Stevens and Huang.
- The method is intuitive and simple to implement.
- The version allow add and remove Material, changing the cross section Area of the bars.
- The material must be gradually removed.
- The variations are made by constant discrete values of the cross section Area  $A_i$ .
- The method is based on the gradient analysis.

## Basic reference



In the discrete form, the problem of compliance  $C$  minimization with weight constraint  $g_w$ , can be written as:

$$\begin{aligned} \text{Minimize} \quad & C = \mathbf{F}_g^T \mathbf{u}_g \\ \text{Subjectto} \quad & \mathbf{K}_g(A_e) \mathbf{u}_g = \mathbf{F}_g \\ & g_w = \sum_{e=1}^{nel} A_e L_e \rho_e \leq W_{lim} \\ & A_{min} \leq A_e \leq A_{max} \end{aligned} \tag{3}$$

where,

- $C$  is the Compliance (objective function);
- $\mathbf{F}_g$  is the nodal force vector;
- $\mathbf{u}_g$  is the nodal displacement vector;
- $\mathbf{K}_g(A_e)$  is the global stiffness matrix ;
- $A_e$  is the elemental cross section area;
- $L_e$  is the elemental length;
- $\rho_e$  is the material density of the element  $e$ ;
- $W_{lim}$  is the limit value of the total weight of the truss;
- $A_{min}$  and  $A_{max}$  are the box constraints, lower and upper limits.



The Compliance minimization is equivalent to Stiffness maximization problem. The objective function of this problem is:

$$C = \frac{1}{2} \mathbf{F}_g^T \mathbf{u}_g \quad (4)$$

where  $C$  is the structure Compliance,  $\mathbf{F}_g$  is the constant external loads and  $\mathbf{u}_g$  is the structural displacement. We consider that the structure is modeled by Finite Element Method, and the static equilibrium equation can be written by:

$$\mathbf{K}_g \mathbf{u}_g = \mathbf{F}_g \quad (5)$$

Introducing the design variable  $A_e$ , as area cross section for the element  $e$ , the strain energy can be re-written, for the cases where the stiffness matrix is symmetric, by:

$$C = \frac{1}{2} \mathbf{F}_g^T \mathbf{u}_g(A_e) = \frac{1}{2} \mathbf{u}_g(A_e)^T \mathbf{K}_g(A_e) \mathbf{u}_g(A_e) \quad (6)$$

where  $A_e$  is the vector of bars cross section area,  $e$  indicate a specific element,  $nel$  is total number of elements. To simplify the notation we use  $\mathbf{K}_g(A_e) = \mathbf{K}_g$  and  $\mathbf{u}_g(A_e) = \mathbf{u}_g$ . But, since  $\mathbf{K}_g \mathbf{u}_g = \mathbf{F}_g$  if  $\mathbf{F}_g$  is constant, than, the first derivative of the equilibrium equation with respect to the design variables  $A_e$  is:

$$\frac{d\mathbf{K}_g}{dA_e} \mathbf{u}_g + \mathbf{K}_g \frac{d\mathbf{u}_g}{dA_e} = 0 \quad (7)$$

than:

$$\mathbf{K}_g \frac{d\mathbf{u}_g}{dA_e} = -\frac{d\mathbf{K}_g}{dA_e} \mathbf{u}_g \quad (8)$$

and,

$$\frac{d\mathbf{u}_g}{dA_e} = -\mathbf{K}_g^{-1} \frac{d\mathbf{K}_g}{dA_e} \mathbf{u}_g \quad (9)$$

And calculating the derivative of  $C$  we have:

$$\frac{dC}{dA_e} = \frac{1}{2} (2 * \mathbf{u}_g^T \mathbf{K}_g \frac{d\mathbf{u}_g}{dA_e} + \mathbf{u}_g^T \frac{d\mathbf{K}_g}{dA_e} \mathbf{u}_g) \quad (10)$$

Replacing the equation (9) in (10) we have:

$$\frac{dC}{dA_e} = \frac{1}{2}(-2 * \mathbf{u}_g^T \mathbf{K}_g \mathbf{K}_g^{-1} \frac{d\mathbf{K}_g}{dA_e} \mathbf{u}_g + \mathbf{u}_g^T \frac{d\mathbf{K}_g}{dA_e} \mathbf{u}_g) \quad (11)$$

and we arrive to:

$$\frac{dC}{dA_e} = -\frac{1}{2} \mathbf{u}_g^T \frac{d\mathbf{K}_g}{dA_e} \mathbf{u}_g \quad (12)$$

The stiffness Matrix variation with respect to the element surface  $A_e$  can be done by:

$$\frac{d\mathbf{K}_g}{dA_e} = \frac{1}{A_e} \mathbf{K}_e \quad (13)$$

where  $\mathbf{K}_e$  is the stiffness matrix of an element  $e$ .

In an displayed form,

$$\frac{d\mathbf{K}_g}{dA_e} = \frac{E}{L} \begin{bmatrix} \lambda^2 & & & \text{Sim.} \\ \lambda\mu & \mu^2 & & \\ -\lambda^2 & -\lambda\mu & \lambda^2 & \\ -\lambda\mu & -\mu^2 & \lambda\mu & \mu^2 \end{bmatrix} \quad (14)$$

we can use the quadratic form, as a positive number that represent the variations of the objective function  $C$  with respect to  $A_e$ :

$$\frac{dC}{dA_e} = \frac{1}{2} \mathbf{u}_e^T \frac{1}{A_e} \mathbf{K}_e \mathbf{u}_e \quad (15)$$

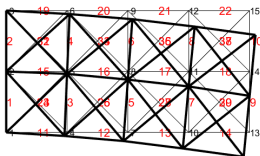
where  $\mathbf{u}_e$  is the displacement vector of one element  $e$ . In this contest, to minimize the compliance, we need decreased the  $A_e$  of the elements with the lowest values of  $\frac{dC}{dA_e}$  and increase the area cross section of the elements with the highest value of the sensitivity function.

The Evolutionary Algorithm can be stated as:

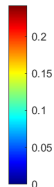
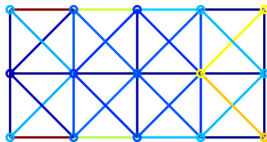
- 1 Discretize the design domain using a finite element method using bars elements. Impose boundary conditions and loads;
- 2 Solve the static structural analysis, finding the nodal displacements;
- 3 Calculate the sensitivity number  $\frac{dC}{dA_e}$ , using the equation 15,
- 4 Reduce the cross section area  $A_e$  by a constant value  $A_e - \delta A_e$  for a fixed number of elements with smaller  $\frac{dC}{dA_e}$  values,
- 5 Increase the cross section area  $A_e$  by a constant value  $A_e + \delta A_e$  for a fixed number of elements with higher  $\frac{dC}{dA_e}$  values,
- 6 Repeat pass 2 and 5 until reach the final volume or an limit value for the compliance.

# Example - cantilever beam

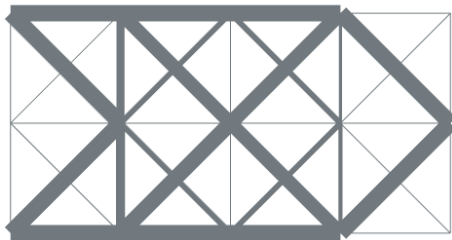
Finite Element Mesh & Max. Displacement [m] = 0.00017927



Sensitivity  $dC/da$



## Finite Element Mesh



## Two-material truss topology optimization for minimum compliance with weight and/or Embodied Carbon constraints.

To implement a two materials models, we need to use a pseudo density variable define as  $x_e$  one value per element. We consider that, if  $x_e = 0$  means that the element is of timber and  $x_e = 1$  means that the element is of steel.

$$\begin{aligned} \text{Minimize} \quad & C = \mathbf{F}_g^T \mathbf{u}_g \\ \text{Subject to} \quad & \mathbf{K}_g(A_e, x_e) \mathbf{u}_g = \mathbf{F}_g \\ & g \leq g_{lim} \\ & A_{min} \leq A_e \leq A_{max} \\ & 0 \leq x_e \leq 1 \end{aligned} \tag{16}$$

The equation (16) can be solve with two different constraints,  $g = g_W$  the weight constraint and  $g = g_{EC}$  the global warning potential. The  $g_{EC}$  is calculated by:

$$g_{EC} = \sum_{e=1}^{nel} = A_e l_e (\rho_e ECC_e) \quad (17)$$

and the limit values are  $W_{lim}$  and  $ECC_{lim}$ . To simulate the material variations we use a material interpolation model: the SIMP model.

$$\begin{aligned} E_e &= (x_e)^p \Delta E + E_{timber} \\ \rho_e &= (x_e)^p \Delta \rho + \rho_{timber} \\ (\rho_e ECC_e) &= (x_e)^p \Delta(\rho ECC) + (\rho ECC)_{timber} \end{aligned} \quad (18)$$

where:

$$\begin{aligned} \Delta E &= E_{steel} - E_{timber} \\ \Delta \rho &= \rho_{steel} - \rho_{timber} \\ \Delta(\rho ECC) &= (\rho ECC)_{steel} - (\rho ECC)_{timber} \end{aligned} \quad (19)$$



## Project definitions:

- Choose one initial truss design, considering two material (steel and Wood) and perform a finite element analysis to find displacements, compliance, weight, and ECC footprint.
- Inspired in the BESO Algorithm, using the gradient information, try to find a solution that minimize the compliance, subject to EEC limit, the equilibrium equation, and box constraints for the area of elements.
- Please, show the intermediate values obtained for objective function and constraints as a function of  $A_e$  and  $x_e$  along the try and error procedure.
- Use the ECO-TOP Matlab script, to perform and to implement one strategy to find a good engineering solution that combine the compliance and the Carbon footprint minimization.
- Write a report with assumed hypotheses and principal obtained results.